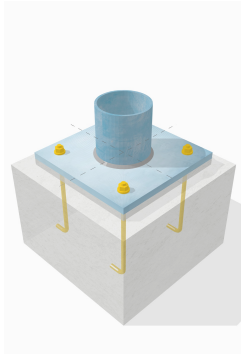
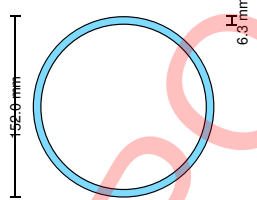
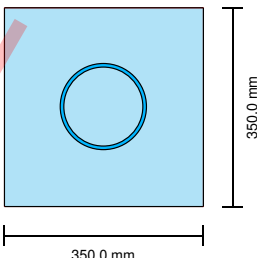
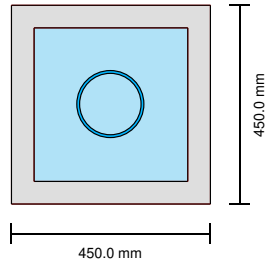
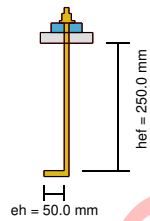


REFERENCES	CALCULATIONS	RESULTS																								
	SkyCiv Base Plate and Anchor Rod Design New Project File Project Information: Design Code: CSA S16:19 and CSA A23.3:19 																									
	Load Combinations: <table><tr><th>Load Combination</th><th>Axial Load, N_x (kN)</th><th>Strong-axis Shear, V_y (kN)</th><th>Weak-axis Shear, V_z (kN)</th></tr><tr><td>1</td><td>100.00</td><td>0.00</td><td>0.00</td></tr></table> Note: Positive N_x (+) indicates compression; negative N_x (-) indicates tension.	Load Combination	Axial Load, N_x (kN)	Strong-axis Shear, V_y (kN)	Weak-axis Shear, V_z (kN)	1	100.00	0.00	0.00																	
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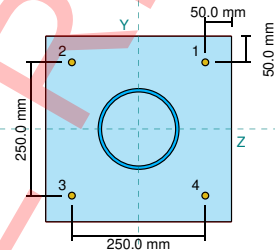
Symbol	Description	Value
B_{conc}	Concrete width	450.0 mm
L_{conc}	Concrete length	450.0 mm
t_{conc}	Concrete thickness	300.0 mm
A_{conc}	Concrete plan area	202500.0 mm ²
f'_c	Concrete compressive strength (20.68)	20.7 MPa
λ	Factor for normal-weight concrete	1.0
—	Concrete assumption: cracked or uncracked	Cracked

Anchor Information:



Symbol	Description	Value
d_a	Anchor rod diameter	12.7 mm
h_{ef}	Anchor rod effective embedment length	250.0 mm
e_h	Anchor hook length	50.0 mm
$F_{y,anc}$	Anchor rod yield stress (ASTM F1554 G36)	248.2 MPa
$F_{t,anc}$	Anchor rod tensile stress (ASTM F1554 G36)	399.9 MPa

Anchor Layout:



Symbol	Description	Value
n_a	Total number of anchor rods	4.0
s_z	Spacing of anchor rods along Z-axis	250.0 mm
s_y	Spacing of anchor rods along Y-axis	250.0 mm
$l_{edge,z}$	Base plate edge distance along Z-axis	50.0 mm
$l_{edge,y}$	Base plate edge distance along Y-axis	50.0 mm

Anchor Data Summary:

ID	Z (mm)	Y (mm)	Anchor in Tension Zone	Breakout (Tension)	Side-Face Blowout (Y-direction)	Side-Face Blowout (Z-direction)
1	125	125	✓	BO Group 1	N/A	N/A
2	-125	125	✓	BO Group 1	N/A	N/A
3	-125	-125	✓	BO Group 1	N/A	N/A
4	125	-125	✓	BO Group 1	N/A	N/A

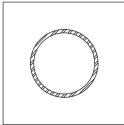
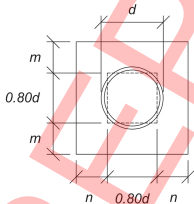
Weld Properties:

Symbol	Description	Value
T_{type}	Weld Type	Fillet
D	Fillet weld size	8.000 mm
t_w	Weld throat	5.657 mm
X_u	Filler metal classification strength (E43XX)	490.000 MPa

Summary of Detailing Checks

Check Name	Dimensions (Min/Max/Actual)	Status
Weld Size Requirement	Min: 8.00 mm, Max: 19.00 mm, Actual: 8.00 mm	PASS
Anchor Clearance	Min: 30.16 mm, Actual: 93.00 mm	PASS
Base Plate Edge Distance	Min: 20.00 mm, Actual: 50.00 mm	PASS
Minimum Number of Anchors	Min: 4.00, Actual: 4.00	PASS
Min. Anchor Spacing to Prevent Concrete Splitting	Min: 50.80 mm, Actual: 250.00 mm	PASS
Min. Concrete Cover to Prevent Concrete Splitting	Min: 75.00 mm, Actual: 100.00 mm	PASS

The design geometry meets requirements!

REFERENCES	CALCULATIONS	RESULTS
CSA S16:19 Clause 13.10, Finished bearing plate per CSA S16:19 Clause 28.5	Load Combination No. 1: Compression Load Only Check No. 1: Column Bearing Capacity Calculate bearing load on column member $N_x = 100 \text{ kN}$ - Compression load B_f - Factored bearing load on steel $B_f = N_x = 100 \text{ kN}$  Fig. Bearing area of column. Calculate bearing capacity of column member $F_{y,col} = 230 \text{ MPa}$ - Column yield stress (230G) $A_{col} = 2910 \text{ mm}^2$ - Column area $\phi = 0.9$ - Structural steel resistance factor B_r - Factored bearing resistance of steel $B_r = 1.50\phi F_{y,col} A_{col} = 1.5 \times 0.9 \times 230 \text{ MPa} \times 2910 \text{ mm}^2 = 903.55 \text{ kN}$ Result: DCR - Demand over capacity ratio: $DCR = \frac{B_f}{B_r} = \frac{100 \text{ kN}}{903.55 \text{ kN}} = 0.11067$	PASS = 0.11
	Check No. 2: Weld Capacity Calculation Note: Calculation of strength is not required since load is transferred via direct bearing. Refer to code for minimum weld size requirements.	N/A = 0.00 Ensure column is FIT-TO-BEAR on the base plate. Refer to CSA S16.19 Clause 28.5.
AISC Design Guide 01 3rd Ed. Section 4.3.1 AISC Design Guide 01 3rd Ed. Section 4.3.1 AISC Design Guide 01 3rd Ed. Section 4.3.1 CSA S16:19 Clause 13.5	Check No. 3: Base Plate Yield Capacity (Compression Load)  Fig. Cantilever lengths of base plate. Calculate critical cantilever length for Round HSS column $d_{col} = 152 \text{ mm}$ - Column outside diameter $L_{bp} = 350 \text{ mm}$ - Base plate length $B_{bp} = 350 \text{ mm}$ - Base plate width l - Critical cantilever length of base plate $l = \max \left(\frac{L_{bp} - 0.8d_{col}}{2}, \frac{B_{bp} - 0.8d_{col}}{2} \right)$ $l = \max \left(\frac{350 \text{ mm} - 0.8 \times 152 \text{ mm}}{2}, \frac{350 \text{ mm} - 0.8 \times 152 \text{ mm}}{2} \right) = 114.2 \text{ mm}$ Calculate applied moment load per unit length on critical section of base plate due to compression from concrete $N_x = 100 \text{ kN}$ - Compression load $B_{bp} = 350 \text{ mm}$ - Base plate width $L_{bp} = 350 \text{ mm}$ - Base plate length $l = 114.2 \text{ mm}$ $m_f = \left(\frac{N_x}{B_{bp} L_{bp}} \right) \left(\frac{l^2}{2} \right)$ $m_f = \left(\frac{100 \text{ kN}}{350 \text{ mm} \times 350 \text{ mm}} \right) \times \left(\frac{114.2 \text{ mm}^2}{2} \right) = 5.3231 \text{ kN} \cdot \text{mm/mm}$ Calculate flexural yielding capacity of base plate per unit length due to compression from concrete $F_{y,bp} = 230 \text{ MPa}$ - Base plate yield stress $t_{bp} = 20 \text{ mm}$ - Base plate thickness $\phi = 0.9$ - Structural steel resistance factor m_r - Factored bending resistance of base plate per unit length	

$$m_r = \phi \left(\frac{(t_{bp})^2}{4} \right) F_{u_{bp}} = 0.9 \times \left(\frac{(20 \text{ mm})^2}{4} \right) \times 230 \text{ MPa} = 20.7 \text{ kN} \cdot \text{mm/mm}$$

Result:

DCR - Demand over capacity ratio:

$$DCR = \frac{m_f}{m_r} = \frac{5.3231 \text{ kN} \cdot \text{mm/mm}}{20.7 \text{ kN} \cdot \text{mm/mm}} = 0.25716$$

PASS = 0.26

Check No. 4: Concrete Bearing Capacity

Calculate bearing load on concrete

$N_x = 100 \text{ kN}$ - Compression load

P_f - Factored bearing load on concrete

$$P_f = N_x = 100 \text{ kN}$$

The restraining side is equal along the concrete width and concrete length.

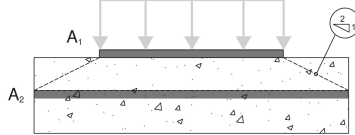


Fig. Bearing area on base plate (A1) and maximum support area on concrete (A2).

Calculate bearing area on base plate

$L_{bp} = 350 \text{ mm}$ - Base plate length

$B_{bp} = 350 \text{ mm}$ - Base plate width

A_1 - Area of bearing on base plate (assume full area)

$$A_1 = L_{bp} B_{bp} = 350 \text{ mm} \times 350 \text{ mm} = 122500 \text{ mm}^2$$

Calculate maximum bearing area on concrete foundation

$N_{A2} = 450 \text{ mm}$ - Length of max bearing area on support (A2)

$B_{A2} = 450 \text{ mm}$ - Width of max bearing area on support (A2)

A_2 - Maximum area of bearing on concrete (assume 1:2 slope)

$$A_2 = N_{A2} B_{A2} = 450 \text{ mm} \times 450 \text{ mm} = 202500 \text{ mm}^2$$

Calculate bearing capacity of concrete

$f'_c = 20.68 \text{ MPa}$ - Concrete compressive strength (20.68)

$$A_1 = 122500 \text{ mm}^2$$

$$A_2 = 202500 \text{ mm}^2$$

$\phi = 0.65$ - Concrete resistance factor

P_r - Factored bearing resistance of concrete

$$P_r = 0.85 \phi (f'_c) A_1 \left(\min \left(\sqrt{\frac{A_2}{A_1}}, 2 \right) \right)$$

$$P_r = 0.85 \times 0.65 \times (20.68 \text{ MPa}) \times 122500 \text{ mm}^2 \times \left(\min \left(\sqrt{\frac{202500 \text{ mm}^2}{122500 \text{ mm}^2}}, 2 \right) \right) = 1799.5 \text{ kN}$$

Result:

DCR - Demand over capacity ratio:

$$DCR = \frac{P_f}{P_r} = \frac{100 \text{ kN}}{1799.5 \text{ kN}} = 0.05557$$

PASS = 0.06

AISC 360-22 Chapter J8, ACI 318-19 Sect. 22.8.3.2 and Fig. R22.8.3.2

AISC 360-22 Chapter J8, ACI 318-19 Sect. 22.8.3.2 and Fig. R22.8.3.2

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CSA A23.3:19 Clause 28.5

REFERENCES	CALCULATIONS	RESULTS																														
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Load Combination	Design Check	Demand	Capacity	DCR	Result																											
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